TWELFTH INTERNATIONAL MAGNET MEASUREMENT WORKSHOP ESRF, Grenoble, FRANCE, October 1-4, 2001

## Insertion Device Magnetic Measurement at Sincrotrone Trieste

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## Specifications for Hall plate bench

- Main axis (Z) :

Travel range 5.5 m , motorised
Pitch, roll and yaw : $\pm 20 \mu \mathrm{rad}$.
Straightness and flatness : $\pm 50 \mu \mathrm{~m}$, measured at a distance of 0.5 m . from the carriage surface any direction.

Encoder resolution $1 \mu \mathrm{~m}$.
Velocity 1-50 mm/sec.
The supplier had to specify the positioning accuracy and the measuring accuracy
(at distance of 0.5 m from carriage surface), over the full travel, and in addition per metre.

- Subsidiary axes : X (horizontal) and Y (vertical), mounted at 90 deg.

Travel range 200 mm , motorised.
Orthogonality of all three axes $\pm 50 \mu \mathrm{rad}$.
Straightness and flatness specified by the supplier.
Encoder resolution $1 \mu \mathrm{~m}$.
The mid-point of the vertical translation stage $(\mathrm{Y})$ must be positioned at 1.2 m above the floor.

The system include the possibility to make in-flight measurements: during a Z-scan
(without stopping) the electronic system is able to generate a TTL signal (trigger) to 2 voltmeters
at predefined equispaced measuring positions. The starting/final points,
trigger position, is programmable via computer (GPIB or RS-232).

## Stretched wire and Hall plate bench



EU6 during magnetic measurements


## Elliptical IDs Installed :

| Period <br> $(\mathrm{mm})$ | Np | Horizontal <br> Polarization | Circular <br> Polarization | Vertical <br> Polarization |
| :--- | :--- | :--- | :--- | :--- |


|  |  | $\mathrm{B}_{0}$ (T) | K | $\varepsilon_{1}(\mathrm{eV})$ | $\mathrm{B}_{0}(\mathrm{~T})$ | K | $\varepsilon_{1}(\mathrm{eV})$ | $\mathrm{B}_{0}(\mathrm{~T})$ | K | $\varepsilon_{1}(\mathrm{eV})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 48(EU) | 44 | 0.57 | 2.58 | 185 | 0.29 | 1.30 | 294 | 0.33 | 1.51 | 371 |
| 60 (EU) | 36 | 0.78 | 4.41 | 59 | 0.42 | 2.39 | 94 | 0.51 | 2.87 | 123 |
| 77(EU) | 28 | 0.91 | 6.56 | 22 | 0.53 | 3.85 | 32 | 0.65 | 4.69 | 42 |
| $\begin{aligned} & 100(E U) \\ & \left.l^{1}\right) \end{aligned}$ | 20 | 1.01 | 9.45 | 8 | 0.63 | 5.85 | 10 | 0.78 | 7.27 | 12 |
| 125(EU) | 17 | 0.78 | 9.06 | 8 | 0.47 | 5.48 | 10 | 0.60 | 7.04 | 12 |
| 212 <br> (EEW) <br> ${ }^{2}$ ) | $\begin{aligned} & \text { 32V, } \\ & \text { 31H } \end{aligned}$ | 0.59 | 10 |  |  |  |  | 0.11 | 2 | 12 |

() Used for a combined SR beamline + S.R. FEL experiment ( 2 undulators)
( ${ }^{2}$ ) Elliptical Electromagnetic wiggler, with variable elicity ( $5 \mathrm{eV}, 1.3 \mathrm{KeV}$ ), max. 100 Hz


## Hall plate bench: description

- The new Hall plate bench, supplied by Microcontrole-Newport (France), was installed in November 1997. It is based on long granite beams of 6.5 m . The bench lies on 12 leveling devices, regulated during the bench installation in order to meet the specified angle tolerances. A carriage moves (Z-axis) on air-bearing along the upper beam, driven by a belt system and a dc-motor (UE512CC). The length of travel of Z axis is 5.5 m . This carriage supports the X (horizontal) and Y (vertical) stages, each with 200 mm of travel, driven by stepping motors (MTL200P1). The total moving mass is about 225 Kg . and the max. Z speed is $60 \mathrm{~mm} / \mathrm{sec}$. The mass of the complete system is about 3.5 tons. The X and Y positions are measured by a rotary encoder, with a sensitivity of $1 \mu \mathrm{~m}$, the Z position is read by a linear encoder (Heidenhain, model Lida $105+$ Exe), having a sensitivity of $1 \mu \mathrm{~m}$.
- All axes are driven by a standard MM4005 Newport integrated motion/controller connected to a PC via RS232 (or GPIB). This controller has the possibility to make inflight measurements: during a Z-scan it is able to generate TTL signals (trigger) to 2 voltmeters (HP-3458) at predefined and equispaced measuring positions.
- Data taking is performed at $20 \mathrm{~mm} / \mathrm{sec}$; the data are stored in the voltmeter buffer and read at the end of the scan.
- First figure: measurements carried out using an electronic level (roll) and an autocollimator (pitch and yaw). It can be seen that the angle errors are within the tolerances specified, apart from a pitch value ( $24 \mu \mathrm{rad}$ ) but measured at the limit of the range ( 5.4 m .). For the old Hall plate bench we measured angle errors about twice larger, along the $2.5 \mathrm{~m} . \mathrm{Z}$ axis.
- Second picture : the difference between the true displacement measured with a HP interferometer and the value given by the motion controller (Heidenhain encoder) as a function of the Z position. The positioning accuracy measured is about 2 times better than specifications (and 4 times the specification for the old bench).
- The squareness between the 3 axes has been measured by a reference granite cube and was better than $50 \mu \mathrm{rad}$.



## HP System performance - REPRODUCIBILITY (rms)

- CLRC array
(By peak 0.76 T , per.200mm)
$\mathrm{L}=1 \mathrm{~m}$, scan 1.4

EEW
$(\mathrm{Bx}, \mathrm{y}$ peak $=0.1,0.6 \mathrm{~T})$
$\mathrm{L}=3.2 \mathrm{~m}$, $\operatorname{scan} 3.8 \mathrm{~m}$

I(Gm)
H. V.
0.019 / 0.034
0.041 / 0.129

II ( $\mathrm{Gm}^{2}$ )
H. V.
0.002 / 0.016
0.010 / 0.037

With this bench, the overall reproducibility is improved: for Ix seems 10 times better (even though now the length of the scan is doubled)
( Old HP bench $\mathrm{Ix}, \mathrm{y}, \mathrm{rms}=0.17,0.15 \mathrm{Gm}$, scan 2.5 m )

EEW : 8 trajectories, calculated from mag.meas. (EEW at max. current) at e-beam 2 GeV
max. peak-peak posit.variation at wiggler exit : $10 \mu \mathrm{~m}$, integration 3.8 m


## Stretched wire bench (for first and second field integral)

- It can be used for MULTIPOLE Field Integral Measurements
- Positioned in the front of the HP bench, ... to be able to perform magn. meas. with both benches without having to move Ids
- 2 indipendent tables support the motorized stages with econdersof $1 \mu \mathrm{~m}$
- Litz wire, 40 strands, wire length $4.2 \mathrm{~m}+$ Integrator
- Typical reproducibility $(\mathrm{rms})===>\mathrm{I}=0.02 \mathrm{Gm}$ and $\mathrm{II}=0.01 \mathrm{Gm}^{2}$


FEL1 und. Period 100 mm , Gap 19, Phase 50.18 mm

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## Correction for the Hall plate planar effect

- EU6 at phase 0 (only By)
- Extract planar coef. for Hor. HP (Bx)
- Fit : Bx,meas $=a_{0}+B y^{*} a_{1}+B y^{2 *} a_{2}$
- Gap $19>\mathrm{a}_{2}=4.6210^{-8}\left(\mathrm{G}^{-1}\right)$

4 runs, rms $0.0310^{-8}\left(\mathrm{G}^{-1}\right)$

- Gap $30>\mathrm{a}_{2}=4.6610^{-8}\left(\mathrm{G}^{-1}\right)$
- Gap $40>\mathrm{a}_{2}=4.110^{-8}\left(\mathrm{G}^{-1}\right)$
- $\mathrm{a}_{1}=<0.1$ deg.
- EU6 at phase $\mathbf{\pm} \mathbf{3 0} \mathbf{~ m m}$ (only Bx)
- Extract planar coef. for Vert.. HP (By)
- Fit: By,meas $=a_{0}+B x * a_{1}+B x^{2 *} a_{2}$
- Found out that the planar coef. was depending on the number of periods used in the fit:
Gap 19 mm
500 pts (ph.pos) $\mathrm{a}_{2}=-1.4 \quad 10^{-7}\left(\mathrm{G}^{-1}\right)$
$260 \mathrm{pts} \quad \mathrm{a}_{2}=+2.010^{-8}\left(\mathrm{G}^{-1}\right)$
$500 \mathrm{pts} \quad(\mathbf{p h} . n e g) \mathrm{a}_{2}=-2.410^{-7}\left(\mathrm{G}^{-1}\right)$
260 pts
$\mathrm{a}_{2}=-1.410^{-7}\left(\mathrm{G}^{-1}\right)$
- $\mathrm{a}_{1}=0.4 \mathrm{deg}$.


## EU4.8 : Hall plate - SW measurements GAP 19 mm



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## EU4.8 : HP - SW measurements GAP 30 mm



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Second field integral APE_1 gap 19 mm , phase 0



EU10 (FEL1) GAP 19 mm , Phase 0 (Bys1 T) Diff. Hor. magn. field with/without HP Planar effect


Effect of planar HP correction (Bx) due to By field
(planar coeff. 4.6e-8 $\mathrm{G}^{-1}$ )

GAP 30 mm , Phase 0 ( $B y=0.7 \mathrm{~T}$ ) Diff. Hor. magn. field with/without HP Planar effect


EEW : Horizontal and vertical first and second field integral, measured on the electron beam and in magn.meas. lab.


- Solid : electron beam
- Dotted : magn.meas.lab.



Electromagnetic Elliptical Wiggler EEW (period $212 \mathrm{~mm}, \mathrm{Bx}, \mathrm{y}=\boldsymbol{\phi} 0.1,0.5 \mathrm{~T}$ )


## EEW - AC measurements

- The flipping coil technique was chosen to perform dynamic measurements (up to 100 Hz ) of field integral variation. i.e. we needed to measure the voltage induced in the static coil by magnetic flux variation, by varying the hor. current.
- Litz wire, 19 strands, stages distance: 4.2 m , connected to HP3458 Voltmeter


Peak to peak field integral variation and rms reproducibility as a function of the integrating time
(aperture) of the voltmeter.

| Freq. <br> $(\mathbf{H z})$ | Apert. <br> $(\mathbf{m S e c})$ | $\Delta \mathbf{I x}$ <br> $(\mathbf{G m})$ | $\mathbf{I x , r m s}$ <br> $(\mathbf{G m})$ |
| :---: | :---: | :---: | :---: |
| 10 | 0.4 | 1.153 | 0.070 |
| 10 | 0.8 | 1.160 | 0.029 |
| 10 | 1.5 | 1.186 | 0.006 |
| 100 | 0.4 | 1.104 | 0.098 |
| 100 | 0.8 | 1.013 | 0.037 |

## ELETTRA Storage ring sensitivity (2 GeV)

- Horizontal plane sensitivity : $14 \mathrm{Gmm} / \mu \mathrm{m}$ closed orbit (rms) (at IDs corr.coils position)
- Vertical plane: $\quad 16 \mathrm{Gmm} / \mu \mathrm{m}$ closed orbit (rms) (at IDs corr.coils position)
- ELETTRA BPMs / Storage ring stability $\approx 1-2 \mu \mathrm{~m}$ rms (closed orbit)
- Accuracy requested for $2-3 \mu \mathrm{~m}$ closed orbit rms
© $0.01-0.03 \mathrm{Gm}$

