

Some aspects of the use of the Vibrating Wire Technique for a wiggler magnetic field measurement.

Alexander Temnykh
Cornell University, USA

1. Introduction
2. Theory
3. Measurement Setup
4. Results
5. Conclusion

Introduction

- Conventional techniques used for wiggler/undulators field and field integral measurement:
 - ◆ Hall probe
 - ◆ Short searching coils
 - ◆ Long flipping coils
- Field measured along **strait** lines is different from field seen by particles moving along **wiggling** trajectory. The difference may cause serious problems for beam dynamics:
 - ◆ J. Safranek et. al., Nonlinear Dynamics in SPEAR Wignglers, Proc. of PAC 1999, New York, pp. 157-161.
 - ◆ D. Alesini et. al., Beam-Beam Experience at DAΦNE, Proc. of PAC 2001, to be published.
- Can we measure field along a wiggling path?
Yes, we can if we use Vibrating Wire Technique.

Theory

- Beam trajectory and displacement of the taut wire with DC current in magnetic field are similar (a well known fact).

$$\frac{\partial^2 X_b}{\partial z^2} = \frac{q}{P} B(z); \quad T \frac{\partial^2 X_w}{\partial z^2} = -I_{dc} B(z)$$

X_b – beam trajectory; X_w – taut wire displacement;

q, P – particles charge and momentum; T, I_{dc} – the wire tension and DC current

if $\frac{I_{dc}}{T} = -\frac{q}{P}$ the wire will imitate beam trajectory.

Theory

- Vertical wiggler magnetic field: $B(z) \approx B_w(z) \sin\left(\frac{2\pi z}{d}\right)$
- The wire wiggling: $X(z) \approx A_w \sin\left(\frac{2\pi z}{d}\right)$ where $A_w = \frac{I_{dc} B_w}{T} \left(\frac{2\pi z}{d}\right)^2$
- Effect of the horizontal field appearance due to the wiggling ($x=0$)

$$B_x(x=0, y, z) = B_z(y, z) X'(z) \approx B_w A_w \left(\frac{2\pi z}{d}\right)^2 \sin\left(\frac{2\pi z}{d}\right)^2 y$$

$$\delta I_x(x=0, y) = \int B_x dz = \frac{B_w A_w L}{2} \left(\frac{2\pi z}{d}\right)^2 y; \quad \delta I_y(x=0, y) = 0$$

Theory

- Effect of the wiggling on field components at $z = 0$

$B_p(x)$ – vertical field variation across single pole

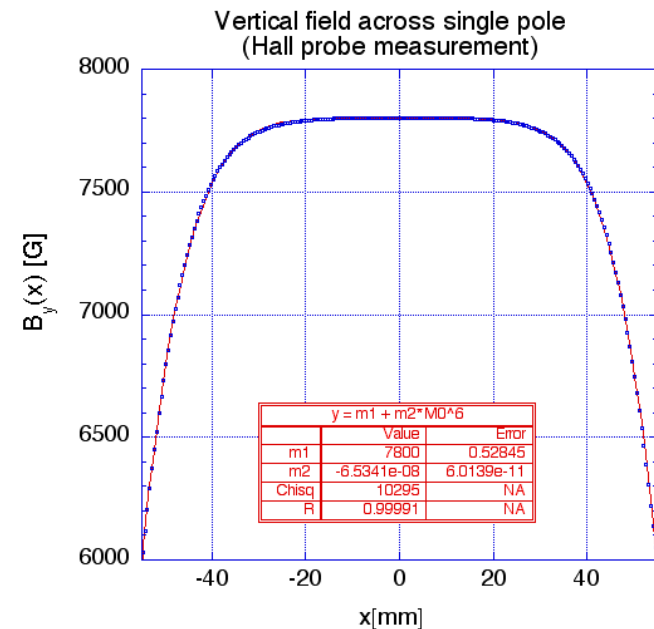
$$\frac{\partial I_x}{\partial x}(x, y = 0) = 0;$$

$$\frac{\partial I_y}{\partial x}(x, y = 0) = \frac{A L}{2 w} \frac{\partial B_p(x)}{\partial x}$$

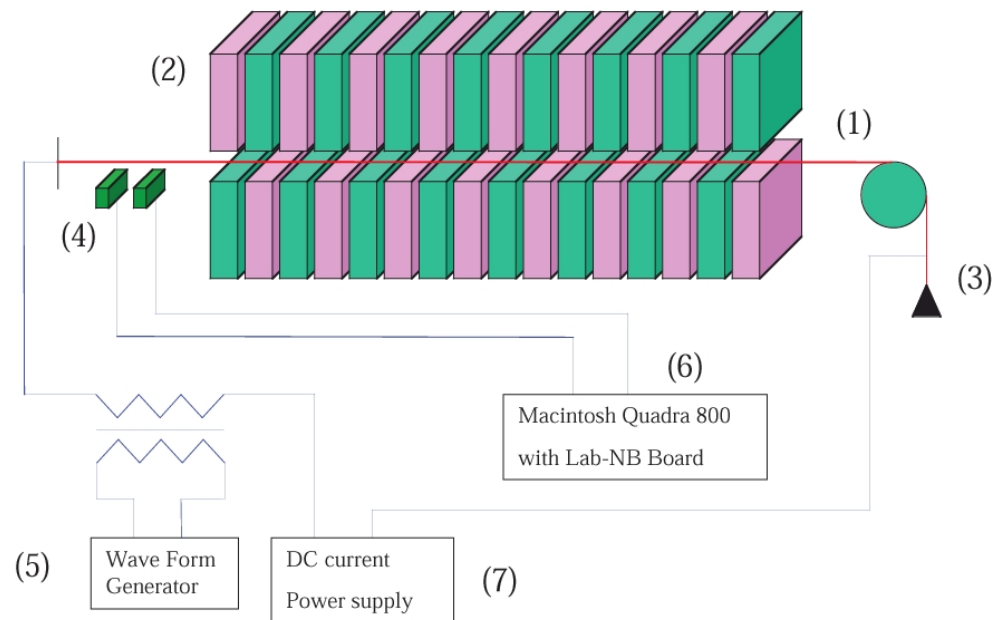
- For experimental condition:

$$B_p(x)[G] = 7.8 \times 10^3 - 6.53 \times 10^{-8} \cdot x^6 [mm]$$

$$\frac{\partial I_y}{\partial x}(x, y = 0)[Gm] = 3.56 \times 10^{-8} \cdot x^5 [mm]$$



Measurement Setup



- (1) 100 micron copper-beryllium wire 382.2 cm in length
- (2) G-line CHESS wiggler, $B_{\max}=0.780\text{T}$, $d=12\text{cm}$, $L=3\text{m}$
- (3) Tension mechanism
- (4) Horizontal and vertical wire position detectors

Results

- Wiggling amplitude calibration with optical means

- Fit:

$$A_w [mm] = (0.255 \pm 0.006) \cdot I_{dc} [A] / T[N]$$

- Model:

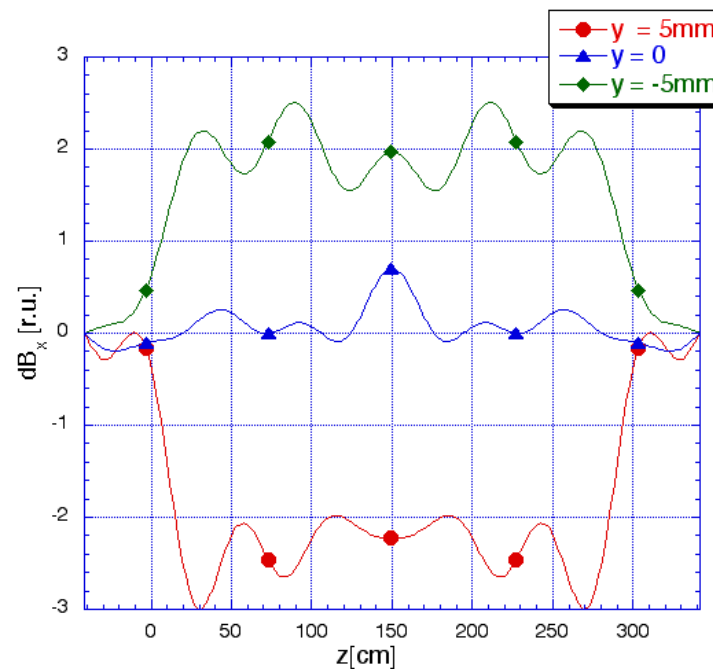
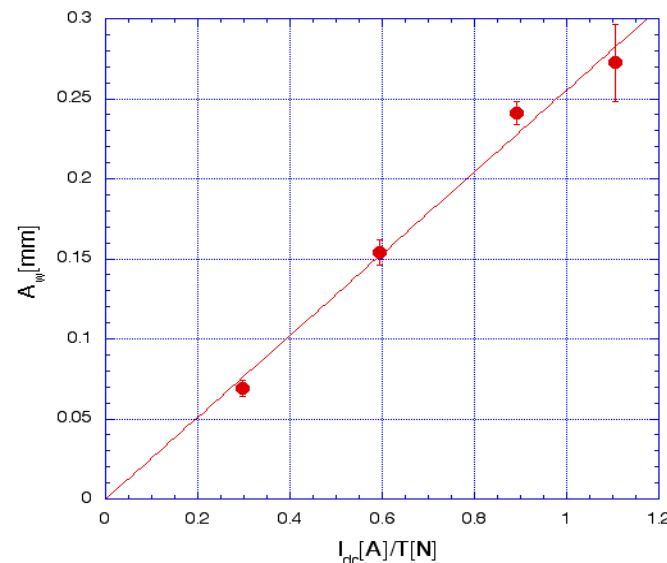
$$A_w [mm] = 0.28 \cdot I_{dc} [A] / T[N]$$

- Difference between horizontal field along z measured with ($A_w=0.124\text{mm}$) and without wiggling ($A_w=0$). 9 odd harmonics were used.

Vertical position $y = -5, 0, 5$ mm

From model $\text{dB}_x \sim 0.8e-3 B_{\text{max}}$

$1[\text{r.u.}] \sim 4e-4 B_{\text{max}}$



Results (theoretical prove)

- If the function of field distribution along magnet is known, one can use only one wire vibrating mode to measure the field integral.

$$\delta B(z) = B_0 \sin\left(\frac{2\pi z}{d}\right)^2; \quad \delta I = \int_0^L \delta B(z) dz = \frac{B_0 L}{2} w$$

Harmonic measured by vibrating wire :

$$H_1 = \frac{2l}{l} \int_0^l \delta B(z) \sin\left(\frac{\pi z}{d}\right) dz = B_0 \frac{2}{\pi} \sin\left(\frac{\pi L}{2l} w\right)$$

The field integral will be :

$$\delta I = H_1 \frac{l}{2} \frac{\pi L}{2l} \sin^{-1}\left(\frac{\pi L}{2l} w\right)$$

- Effect from small shim placed in the middle of magnet and measured with long flipping coil was used for calibration.

Results

- Vertical / horizontal field integrals versus y , $A_w = 0.060\text{mm}$,
 - Measurement

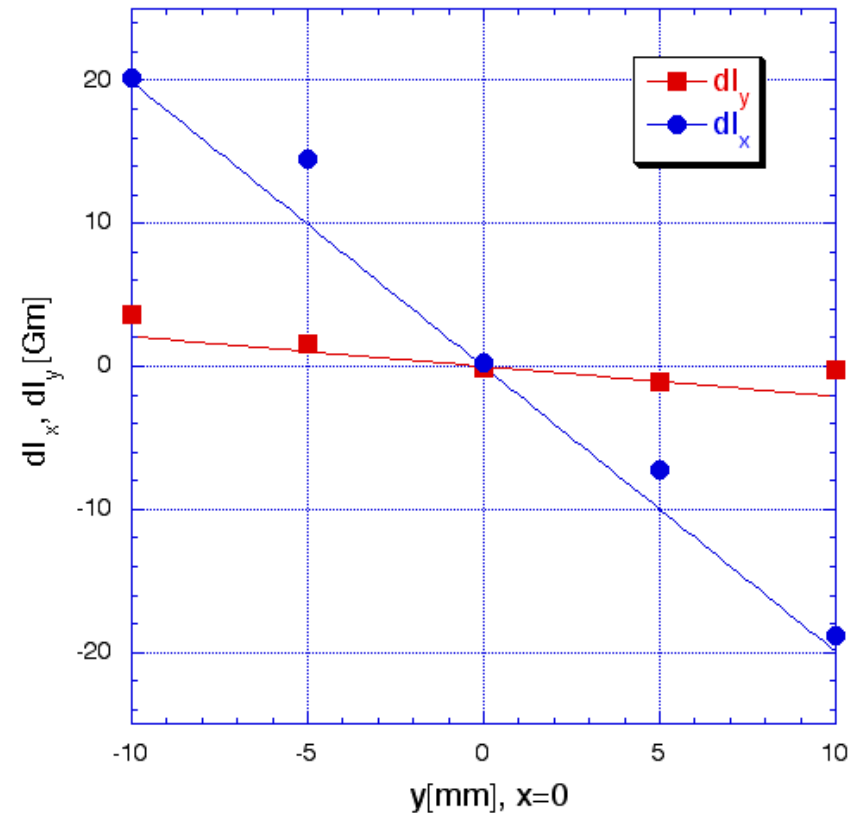
$$\delta I_x(x=0, y)[Gm] = (-1.99 \pm 0.17) \cdot y[mm]$$

$$\delta I_y(x=0, y)[Gm] = (-0.21 \pm 0.08) \cdot y[mm]$$

- Model:

$$\delta I_x(x=0, y)[Gm] = -1.92 \cdot y[mm]$$

$$\delta I_y(x=0, y)[Gm] = 0$$



Results

- Vertical / horizontal field integrals versus x, $A_w = 0.060\text{mm}$,
 - Measurement

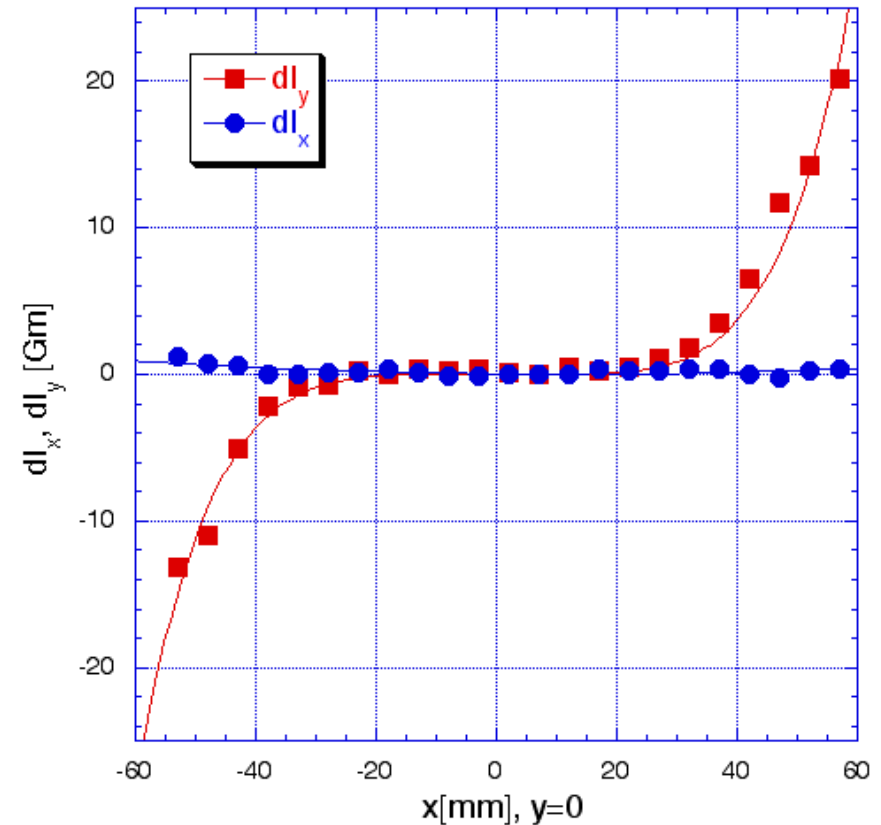
$$\delta I_x(x, y = 0)[Gm] \approx 0$$

$$\delta I_y(x, y = 0)[Gm] = (3.60 \pm 0.12) \cdot x^5 [mm]$$

- Model:

$$\delta I_x(x, y = 0)[Gm] = 0$$

$$\delta I_y(x = 0, y)[Gm] = 3.56 \times 10^{-8} \cdot x^5 [mm]$$



Conclusion

- Vibrating Wire Technique was used to measure field distribution and field integrals along a **wiggling** path imitating beam trajectory.
- Obtained data is in excellent agreement with model calculation.
- The Vibrating Wire Technique has unique features which can be effectively exploited in the Insertion Devices magnetic field measurements.